

RT FORMULAE

$$1. \text{ Geometrical Unsharpness } U_g = \frac{d \cdot t}{SFD - t}$$

Where,

d=effective dia. of the source size

t=thickness of job

SFD= source to film distance

Minimum SFD calculation:

$$SFD = t \left(1 + \frac{d}{U_g} \right)$$

$$2. \text{ Radiation level } R_L = \frac{\text{Activity} \times RHM}{d^2}$$

Where,

RHM = Rontgen per Hour per Meter. d =distance

$$3. \text{ Exposure time} = \frac{\text{film factor} \times SFD^2 \times 2^n \times 60}{Ci \times RHM \times 100^2}$$

Where,

$$n = \frac{x}{HVT}, \quad x = \text{thickness of the job. HVT=Half Value Layer thickness of steel}$$

$$4. \text{ Allowed working Time} = \frac{\text{Dose limit}}{\text{Dose rate}}$$

$$5. \text{ Inverse Square Law: } \frac{I_1}{I_2} = \frac{d_2^2}{d_1^2}$$

Isotopes	Half Life	RHM value	Optimum Working Steel Thickness (mm)
Ir-192	74.4 days	0.55	10-60 mm
Co-60	5.27 years	1.30	50-200 mm
Tm-170	127 days	0.0025	2-10 mm
Cs-137	33 years	0.34	50-125 mm

MT FORMULAE

1. Longitudinal Current Calculation: $NI = \frac{45000}{\frac{L}{D}}$

Where,

L = Length of the component

D = Dia. of the component

2. For stationary equipment, current calculations:
 Circular magnetization for AC : 500 – 800 Amp/Inch
 Circular magnetization for AC : 800 – 1000 Amp/Inch

3. A.S.T.M. Recommended Prod Spacings and current Values.

Prod Spacing, Inches	Section Thickness, Inches	
	Under ¾ inch	¾ inch and over
2 to 4	200 to 300 Amperes	300 to 400 Amperes
Over 4 to less than 6	300 to 400 Amperes	400 to 600 Amperes
6 to 8	400 to 600 Amperes	600 to 800 Amperes

4. Yoke Calibration checks (Weight lifting capacities):
 For A.C Current: 4.5 Kgs for 2 to 6 inch leg spacing
 For D.C Current: 18 Kgs for 100 to 150 mm leg spacing

UT FORMULAE

1. Wave length $\lambda = \frac{V}{F}$

Where,

V = velocity (Km),

F = frequency (MHz)

2. Acoustic Impedance $Z = \rho.V$

Where,

ρ = density Kg/m³,

v = velocity m/sec,

Z = Kg/m²/sec

3. Reflection $R(\%) = \frac{(z_2 - z_1)^2}{(z_2 + z_1)^2}$

Transmission $T(\%) = \frac{4z_2 z_1}{(z_2 + z_1)^2}$

and T+R=1

Where,

Z₁ = Acoustic Impedance – I

Z₂ = Acoustic Impedance – II

4. Snell's law : $\frac{\sin i}{\sin r} = \frac{v_i}{v_r}$

Where,

Sin i = incident angle

Sin r = refracted angle

v_i = Velocity media-I

v_r = Velocity media-II

5. Critical Angle $\sin \theta = \frac{v_1}{v_2}$

Where,

v₁=Velocity media-I

v₂=Velocity media-II

6. Beam spread: $\sin \theta = \frac{1.22\lambda}{D}$

Where,

θ =Half angle of beam spread

λ = Wave length

D=Dia. of the transducer

7. Near field $N = \frac{D^2 F}{4V}$

Where,

D=Dia. of the transducer

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F=Frequency of the transducer

V=Velocity of the material

8. dB Calculation $dB = 20 \log_{10} \frac{H_2}{H_1}$

Where,

H_1 = Echo Height I

H_2 = Echo Height II

$$\frac{H_2}{H_1} = 10^{N/20}$$

Where,

N=dB given

9. Echo Height/ Size / distance :

$$\frac{H_2}{H_1} = \frac{x_2^2}{x_1^2} \times \frac{d_1^2}{d_2^2}$$

Where,

H_1 = Echo Height I

H_2 = Echo Height II

x_1 = Size of defect I

x_2 = Size of defect II

d_1 = Distance of defect I

d_2 = distance of defect II

10. Focal length

$$R = F \frac{(n-1)}{n}$$

Where,

R = Radius of curvature of the lens

F = Focal length of water

n = the ratio of velocity = V_1/V_2

11. Attenuation coefficient

$$\frac{dB}{M} = \frac{(Hx_1 - Hx_2)dB - 20 \log_{10} \frac{x_2}{x_1}}{2(x_2 - x_1)}$$

Where,

$(Hx_1 - Hx_2)dB$ = dB difference

x_1 = Echo height I

x_2 = Echo height II

12. Focused Probe:

$$X_m - (f_w - X_w) \frac{V_w}{V_m}$$

Where,

V_w = Velocity of water km/sec

V_m = Velocity of material Km/sec

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X_m = Metal distance

F_w = Focal width

θ = Angle unit

13. Unfocussed probe $F_w = N_w$

$$N = \frac{D^2 F}{4V}$$

Where,

D = Dia. of the transducer

F = Frequency of transducer

V = Velocity of material

14. Offset distance

$$X - R = \frac{V_w}{V_m} \sin \theta$$

Where,

X = offset distance, R = Radius of the job

V_w = Velocity in water, θ = Refracted angle

V_m = Velocity in material

15. Limiting angle

$$\theta = \sin^{-1} \left(\frac{ID}{OD} \right) \text{ or } \theta = \sin^{-1} \frac{2t}{OD}$$

$$\text{Thickness detected } T = \frac{D}{2} (1 - \sin \theta)$$

Where,

D = Dia. of job

T = Thickness of job

Thickness undetected from ID, $T = \frac{d_1 - d}{2}$

$d_1 = D \sin \theta$

d = ID of job

16. Tandom Technique $X = 2(t - D) \tan \theta$

Where,

X = Probe spacing (mm)

T = Thickness of job (mm)

D = Depth of defect (mm)

θ = Angle unit

17. Velocity measurement

$$\frac{\text{Actual thickness}}{\text{Actual Velocity}} = \frac{\text{Apparent Thickness}}{\text{Calibrated Velocity}}$$

18. Automation

$$a. \text{ PRR} = \frac{n \cdot S}{d_p}$$

Where,

PRR = Pulse Repetition Rate

N = No. of Hits
 S = Speed (m/s)
 D_p = Dia. of probe (mm)
 V = Velocity (Km/sec)

b. $PRR = \frac{V}{2 \cdot x \cdot n}$

Where,

X = thickness
 N = No. of hits
 PRR = Pulse Repetition Rate

19. Time Taken for plate

$$T = \frac{\text{Area of the plate}}{W \cdot S}$$

Where,

W = Scan width
 S = Speed

20. Surface Speed:

$$SI = D_m \times RPS$$

Where,

D_m = Metal Dia.
 RPS = Revolution Per Seconds
 L = Length of the job
 W = Scan width

21. Velocity = $\frac{\text{Distance Travelled}}{\text{Time}}$